

Name: \_\_\_\_\_ Student ID \_\_\_\_\_

**Prince of Songkla University  
Faculty of Engineering**

**Exam: Final Exam, Semester I  
Date: October 12, 2005  
Subject: 230-391 – Basic Chemical Engineering I**

**Academic Year: 2005 – 06  
Time: 13:30 – 16:30  
Room: R300**

**ทฤษฎีในการสอบโทษขั้นต่ำคือ ปรบตกในรายวิชาที่ทฤษฎี แล้ชกการเรียน 1 ภาคการศึกษา**

**Instructions: There are a total of 4 problems. The points for each problem are not distributed evenly. Place your name and the student ID number on every page. Students are allowed to use only a pen or pencil, a calculator, and one page of A4 note front and back into the examination. Student can use the Conversions Table. No exams are allowed to leave the room.**

<b>Points Distribution (For Grader Only)</b>		
<b>Problem</b>	<b>Points Value</b>	<b>Score</b>
<b>1</b>	<b>35</b>	
<b>2</b>	<b>25</b>	
<b>3</b>	<b>15</b>	
<b>4</b>	<b>25</b>	
<b>Total</b>	<b>100</b>	

**Exam prepared by  
Ram Yamsaengsung  
October 5, 2005**

**PLEASE CHECK TO MAKE SURE THAT  
YOU HAVE ALL 5 PAGES OF THE EXAM BEFORE BEGINNING  
(not including the cover sheet).  
GOOD LUCK!**

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1. Eight hundred gal/hr of water is being pumped from a reservoir to a storage tank located 300 meters away. The pipe has an internal diameter of 4.5 cm. Assuming the inside of the pipe is smooth, determine the following information. **(35 Points Total)**
- Determine the average velocity inside the pipe (in m/s). **(5 points)**
  - Is the flow laminar or turbulent ( $\mu = 1 \text{ cp}$  and  $\rho = 1,000 \text{ kg/m}^3$ )? **(5 points)**
  - Determine the pressure drop from the reservoir to the water tank (in Pa). **(10 points)**
  - Determine the power requirement in **horsepower**. Assuming that the initial velocity at point 1 is 0.0 m/s and the final velocity at point 2 is equal to the average velocity inside the pipe. **Begin with the Bernoulli Equation and state all assumptions. (15 points) (There is no sudden expansion and  $e_v$  for  $90^\circ$  elbow = 0.5.)**
  - For Graduate Students ONLY or BONUS for Bio-Tech Students:** Derive the equation for the Shear Stress at the wall of the pipe (at  $r = R$ ). Begin with the velocity profile and show that force at the wall  $F = \Delta P \pi R^2$ . **(10 points)**

Work of Pump is given by:

$$W_p = w\hat{W}$$

where,  $W_p$  = work of pump (convert to hp),  
 $w$  = mass flow rate (kg/s)  
 $\hat{W}$  = work per unit mass ( $\text{m}^2/\text{s}^2$ )

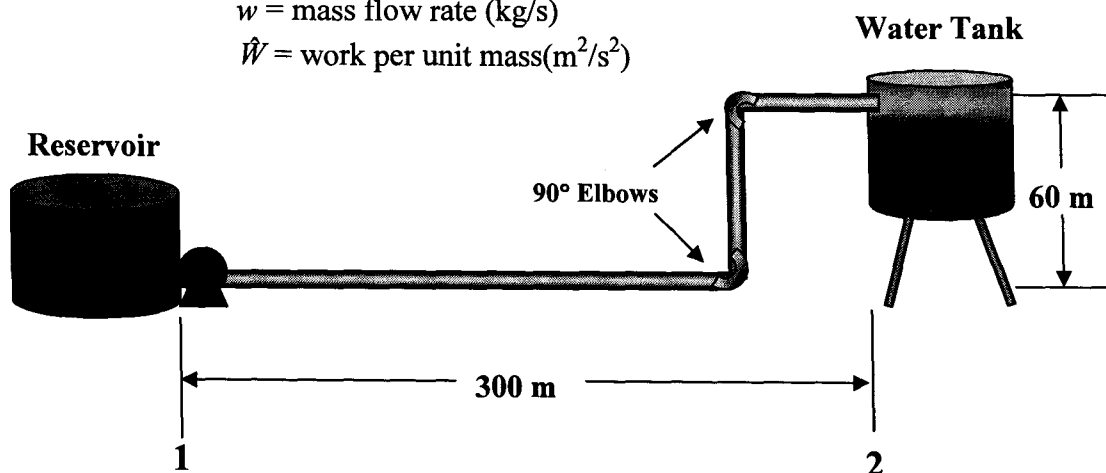


Figure 1: Flow of water through a circular pipe.

2. A viscous incompressible fluid is flowing in a slit formed by two parallel walls a distance  $2B$  apart. **(25 Points Total)**
- (a) What is the Reynolds number of the falling film if the velocity is 10 cm/s, the viscosity is 5 cp, the density is 1.5 g/cm<sup>3</sup>,  $W = 8$  cm,  $B = 0.4$  cm, and  $L = 30$  cm. **(10 points)**
- (b) Make a differential momentum balance and obtain the expressions for the distributions of momentum flux given below: **(15 points)**

$$\tau_{zx} = \left( \frac{P_o - P_L}{L} \right) x$$

where  $P = p + \rho gh = p - \rho gz$

**Hint:** Write a momentum balance (momentum in, momentum out, gravity force, pressure force, shear stress force) then convert it to a differential ( $d\tau_{xz}/dx$ ) by taking the limit as  $\Delta x \rightarrow 0$ .

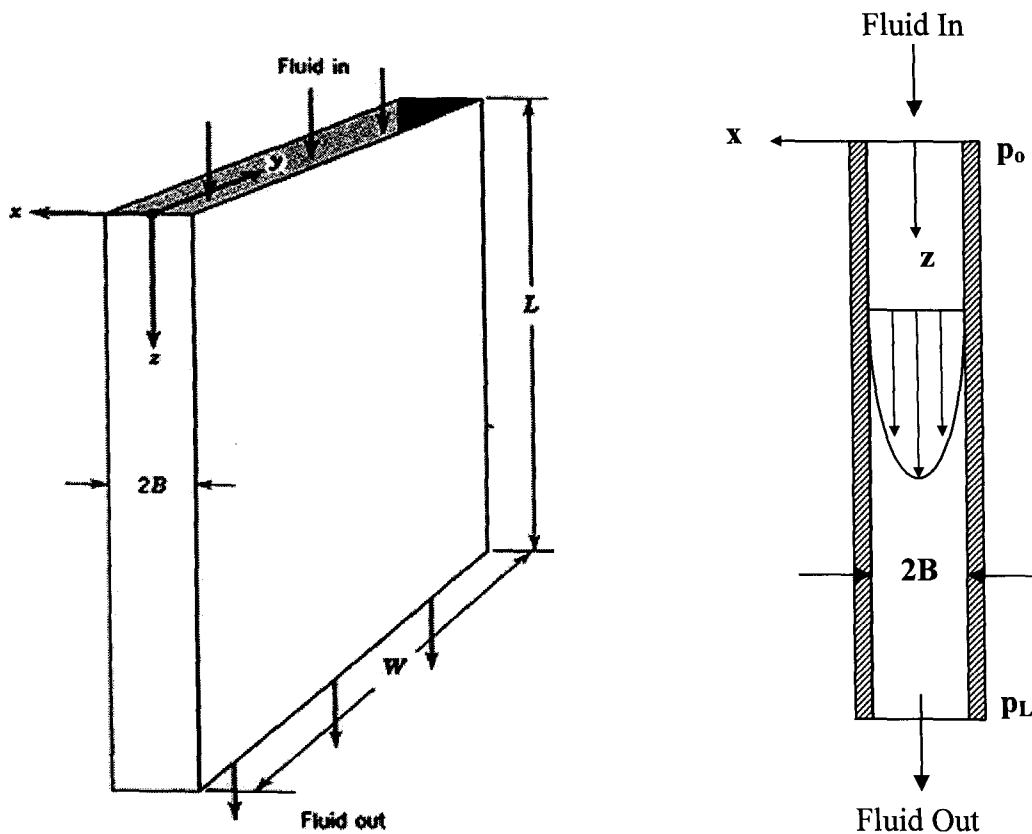


Figure 2: Falling film through a slit.

3. A rotary drum filter is used to filter calcium carbonate from a slurry containing 3.5 lb of dry solid per cubic foot of solid free liquid at a constant pressure difference of 8.5 psi. The specific cake resistance for the slurry and the volume of the filtrate obtained are given by the equations below:

$$\alpha = 1.85\Delta P^{0.3} \quad [\text{lb}_r\text{-h}/(\text{lb}_m\text{-ft})]$$

$$V^2 = \frac{2\Delta P A^2 \theta}{\alpha W}, \text{ where } \Delta P \text{ is in lb}_f/\text{ft}^2$$

Determine the diameter of the filtering drum (in inches) if the width of the drum is 2 feet and 30 ft<sup>3</sup> of filtrate is obtained in 10 minutes. Assuming 1 ft<sup>3</sup> of filtrate is obtained for every cubic foot of solid-free liquid entering the unit. The resistance of the press and the cloth may be neglected, and the filtrate may be assumed to as completely free f all solid materials. **(15 Points Total)**

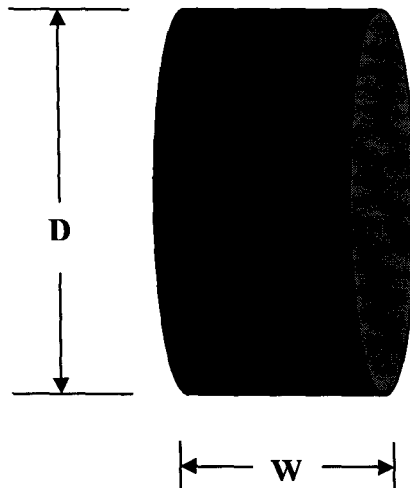


Figure 3: Rotary drum filter.

4. If the density of the fluid is  $1.1 \text{ g/cm}^3$ , the density of particle A is  $9.50 \text{ g/cm}^3$  and the density of particle B is  $2.05 \text{ g/cm}^3$ , answer the following questions: **(25 Points Total)**

- For the particle settling velocity of components A and B shown below, which region will produce a pure fraction of A and which region will produce a pure fraction of B? **(10 points)**
- If the diameter of particle B is  $0.50 \text{ cm}$ , what is the diameter of particle A that is falling at the same rate? **(5 points)**
- What is the terminal velocity of particle A (given  $\mu = 0.50 \text{ cp}$ )? **(10 points)**

Assume that the particle is falling under Newton's Regime and  $C_D = 0.44$ .

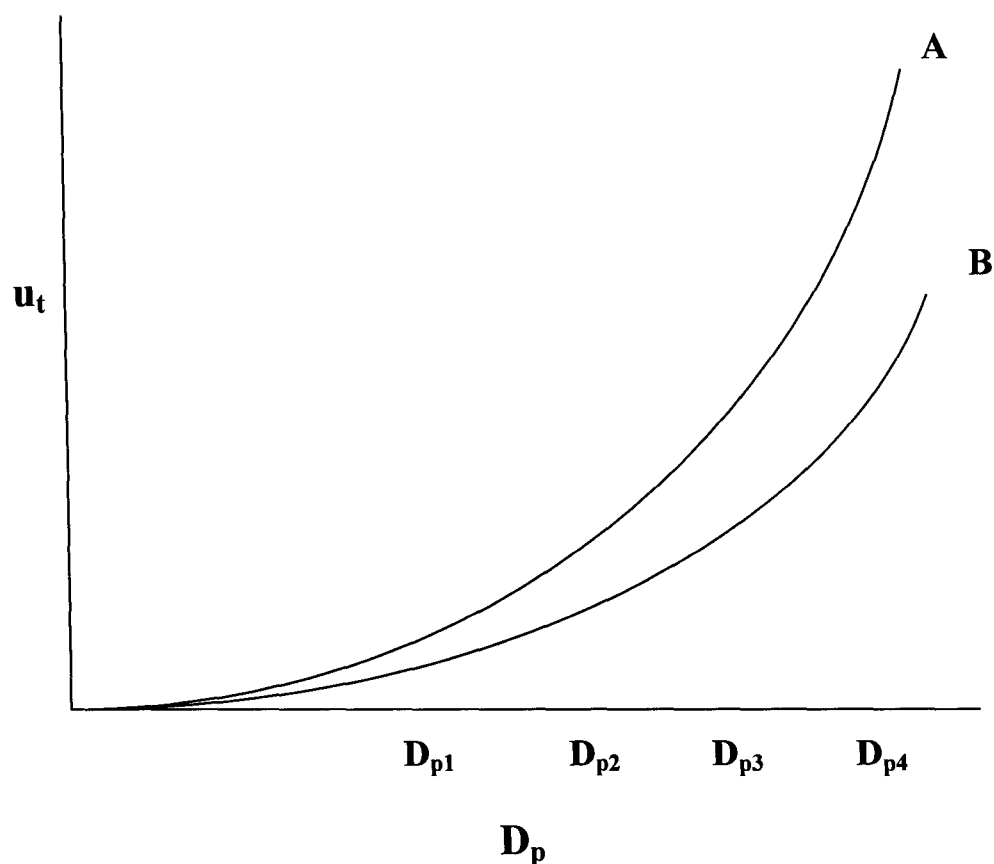


Figure 4: Terminal velocity as a function of particle diameter for components A and B.

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**END OF EXAM!  
CONGRATULATIONS!  
HAVE A GOOD SEMESTER BREAK!**

## Useful Information

<b><u>Conversions:</u></b>	$g_c = 32.2 \text{ ft}\cdot\text{lb}_m / (\text{lb}_f\cdot\text{s}^2)$ $g = 9.81 \text{ m/s}^2$ $1 \text{ lb}_m = 0.454 \text{ kg}$ $1 \text{ psia} = 6.89476 \text{ kPa}$ $1 \text{ m}^3 = 264.172 \text{ gal}$ $1 \text{ N}\cdot\text{m} = 0.737562 \text{ ft}\cdot\text{lb}_f$	$1 \text{ in.} = 2.54 \text{ cm}$ $1 \text{ N} = \text{kg}\cdot\text{m/s}^2$ $1 \text{ cp} = 1 \times 10^{-2} \text{ g/cm}\cdot\text{s}$ $1 \text{ Pa} = 1 \text{ N/m}^2 = 1 \text{ kg/m}\cdot\text{s}^2$ $1 \text{ Btu} = 1055 \text{ J}$ $1 \text{ hp} = 550 \text{ ft}\cdot\text{lb}_f/\text{s}$
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### **Bernoulli Equation:**

$$\Delta \frac{1}{2} \langle \bar{v} \rangle^2 + g\Delta h + \int_{p_1}^{p_2} \frac{1}{\rho} dp + \hat{W} + \sum_i \left( \frac{1}{2} \langle \bar{v} \rangle^2 \frac{L}{R_h} f \right)_i + \sum_i \left( \frac{1}{2} \langle \bar{v} \rangle^2 e_v \right)_i = 0$$

$$\sum_i \left( \frac{1}{2} \langle \bar{v} \rangle^2 \frac{4L}{D} f \right)_i = \frac{2 \langle \bar{v} \rangle^2 f}{D} \sum_i L_i$$

### **Pressure Drop versus friction factor:**

$$\left( \frac{P_0 - P_L}{\frac{1}{2} \rho \langle \bar{v} \rangle^2} \right) = \left( \frac{L}{R_h} \right) f$$

### **Reynold's Number:**

$$N_{Re} = \frac{\rho V D}{\mu}, \text{ where } D = 4R_h$$

### **Flow in Circular Tube:**

$$\tau_{rz} = -\mu \left( \frac{dV_z}{dx} \right) \quad v_z = \left( \frac{(P_0 - P_L) R^2}{4\mu L} \right) \left[ 1 - \left( \frac{r}{R} \right)^2 \right] \quad Q = \left( \frac{(P_0 - P_L) \pi R^4}{8\mu L} \right)$$

### **Terminal Falling Velocity for a Sphere:**

$u_t = \sqrt{\frac{4g(\rho_p - \rho)D_p}{3C_D\rho}}$	$\frac{D_{p,A}}{D_{p,B}} = \sqrt{\frac{\rho_{pB} - \rho}{\rho_{pA} - \rho}}$	<b>Stoke's Regime</b>
$N_{Re,p} = \frac{\rho u_t D_p}{\mu}$	$\frac{D_{p,A}}{D_{p,B}} = \frac{\rho_{pB} - \rho}{\rho_{pA} - \rho}$	<b>Newton's Regime</b>

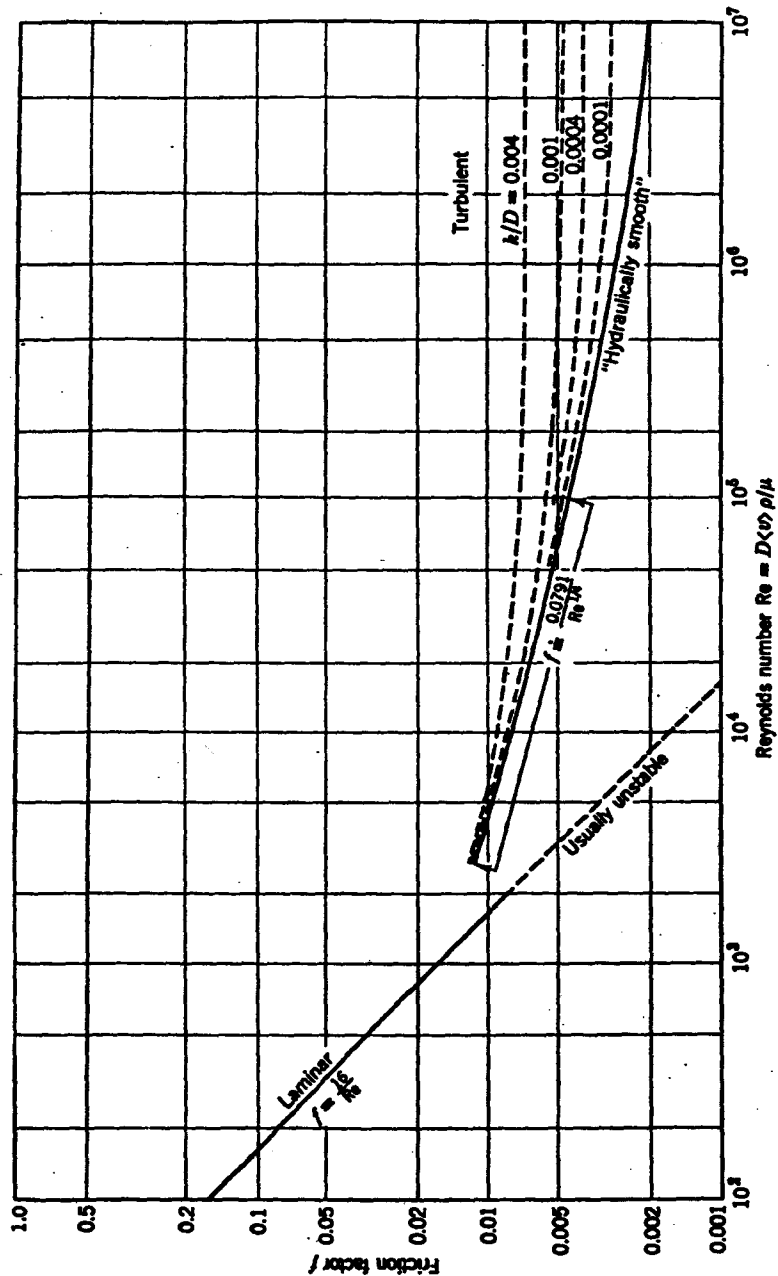


Fig. 6.2-2. Friction factors for tube flow (see definition of  $f$  in Eqs. 6.1-2 and 6.1-3. [Curves of L. F. Moody, *Trans. ASME*, 66, 671 (1944) as presented in W. L. McCabe and J. C. Smith, *Unit Operations of Chemical Engineering*, McGraw-Hill, New York (1954).]

### Estimation of the Friction Loss

Here  $R_h$  is the mean hydraulic radius defined in Eq. 6.2-16,  $f$  is the friction factor defined in Eq. 6.1-4, and  $e_s$  is the friction loss factor given in Table 7.4-1. Note that the  $\langle \bar{v} \rangle$ 's in the first terms refer to the average velocities at the planes "1" and "2"; the  $\langle \bar{v} \rangle$  in the first sum indicates the average velocity in the  $i$ th pipe segment; and the  $\langle \bar{v} \rangle$  in the second sum is the average flow velocity *downstream* from the  $i$ th fitting, valve, or other obstacle.

TABLE 7.4-1  
BRIEF SUMMARY OF FRICTION LOSS FACTORS FOR USE WITH EQ. 7.4-10.  
(Approximate Values for Turbulent Flow)<sup>a</sup>

Obstacles	$e_s$
<b>Sudden Changes in Cross-Sectional Area<sup>b</sup></b>	
Rounded entrance to pipe	0.05
Sudden contraction	$0.45(1 - \beta)$
Sudden expansion <sup>c</sup>	$\left(\frac{1}{\beta} - 1\right)^2$
Orifice (sharp-edged)	$2.7(1 - \beta)(1 - \beta^2) \frac{1}{\beta^2}$
<b>Fittings and Valves</b>	
90° elbows (rounded)	0.4-0.9
90° elbows (square)	1.3-1.9
45° elbows	0.3-0.4
Globe valve (open)	6-10
Gate valve (open)	0.2

<sup>a</sup> Taken from H. Kramers, *Physische Transportverschijnselen*, Technische Hogeschool, Delft, Holland (1958), pp. 53-54.

<sup>b</sup>  $\beta = (\text{smaller cross sectional area})/(\text{larger cross sectional area})$

<sup>c</sup> See derivation from the macroscopic balances in Example 7.5-1. When  $\beta = 0$ ,  $E_s = \frac{1}{2}(\bar{v})^2$  where  $\langle \bar{v} \rangle$  is the velocity *upstream* from the enlargement.

### Example 7.4-1. Power Requirements for Pipe-Line Flow

What is the horsepower needed to pump the water in the system shown in Fig. 7.4-1? Water ( $\rho = 62.4 \text{ lb}_m \text{ ft}^{-3}$ ;  $\mu = 1.0 \text{ cp}$ ) is to be delivered to the upper tank at a rate of  $12 \text{ ft}^3 \text{ min}^{-1}$ . All of the piping is 4-in. internal diameter smooth circular pipe. Assume that the pipes run full of liquid.

**Solution.** The average velocity in the pipe is

$$\langle v \rangle = \frac{Q}{\pi R^2} = \frac{(12/60)}{\pi(1/6)^2} = 2.30 \text{ ft sec}^{-1}$$